

Performance Evaluation of Waterflood Reservoirs in High Water Cut Period Based on New Relative Permeability Model

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Abstract: Water flooding performance evaluation and recovery prediction with relatively easy tools has always been among the top aims of reservoir engineering studies, especially for mature reservoirs in high water-cut period. Relative permeability curves are basic required properties reflecting multi-phase flow characteristic and used together with production history to evaluate reservoir performance. In high water-cut period the relative permeability ratio deviate from the empirical straight-line form, which makes traditional models less effective or erroneous in performance prediction. This paper presents a new relative permeability ratio model which can convert the non-linear characteristic of this problem into linear expression. And a new simple water flooding performance analysis technique is developed based on the new model, which can be used to forecast ultimate recovery factor and the corresponding sweep efficiency. The main advantage of this work is taking into account of high water-cut characteristic with less model parameters compared with other improved models. Synthetic case and field examples demonstrated the advantages of this method in parameter solving and consistency in history matching. The proposed technique in this work can be used as predictive analysis tool in forecasting ultimate recovery and performance evaluation for mature water flooding reservoirs.

Keywords: Water Flooding Performance, Relative Permeability, Recovery Factor, High Water-cut

1. Introduction

Many sophisticated simulation software are available in water flooding performance evaluation and recovery prediction, nevertheless petroleum engineers are still in need of simple tools or correlations for dynamic analysis due to time-consuming or data shortage. Pure “data-driven” analysis of reservoir performance cannot reasonably interpret the nature of multi-phase flow in reservoirs and may bring wrong predictions even under a good history match study. So the use of relative permeability together with production history provides an effective way in reservoir performance evaluation, combining flow mechanism and production practice.

Over the past decades of years water-oil ratio (WOR) analysis has been widely used for performance evaluation and production forecasting for water flooding reservoirs. Some empirical relations have been presented and accepted

in oil field practice.

Ershagi and Omoregie [1] presented a recovery ratio and water-cut relation called “X-plot”, as shown in equation (1), based on the concepts of fractional flow and the frontal advance theory (Buckley and Leverett), which can predict recoverable oil volume by extrapolating the curve to arbitrary value of water-cut (f_w).

$$E_r = a_{er} + b_{er}X \quad (1)$$

In equation (1) E_r is the recovery ratio, which can be calculated by cumulative oil production divided by oil in place (N_p/N), X is a function of water-cut (f_w), and the constants a_{er} and b_{er} have dependency on a linear relative permeability ratio relation as described in Appendix 1.

Lo [2] suggested using a logarithm relationship of WOR and N_p , in which the coefficient constants can be determined by the straight-line relationship of relative permeability ratio and water saturation either, as described in Appendix 2.

Over the past decade some researchers began to realize that the straight-line relationship would not exist when water saturation is close to large value in late production stage of oilfield as shown in Figure 1. In high water-cut period the relative permeability ratio deviate from the empirical straight-line form, which makes traditional models less effective or erroneous in performance prediction, leading to an over-estimation of recoverable oil.

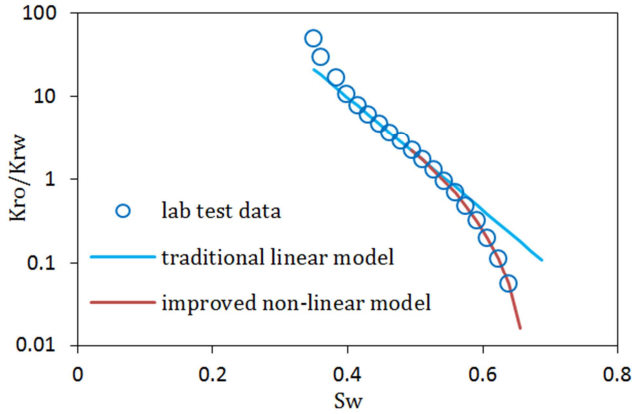


Figure 1. Non-linear match of relative permeability ratio.

Yortos, et al. [3] divided the relative permeability curve into two separate regions, as “exponential” and “power-low” region. B. Can [4] proposed a nonlinear relative permeability ratio relation and presented a modified Y-Function model to evaluate performance of water following. Nevertheless, the application comparison of the modified Y-function model with other five commonly used models did not show any advantage over Arp’s decline model. Other researchers [5-7] provided different models for the relative permeability ratio and developed different performance prediction models, shown in Table 1. These improved models have not obtained wide application because of tedious unknown-parameter matching and solving problems or generating inconsistency with real reservoir performance.

Table 1. List of the non-linear relative permeability ratio models.

Year	Author	Relative Permeability Ratio Model
2011	LIU S.	$k_{ro}/k_{rw} = ae^{-b \cdot c^{S_w}}$
2013	Song Z.	$k_{ro}/k_{rw} = de^{-(aS_w^2 + bS_w)}$
2013	HOU J.	$\ln(k_{ro}/k_{rw}) = m + nS_w + pe^{S_w}$
2014	B. Can	$k_{ro}/k_{rw} = Ae^{-BS_w^C}$

2. New Model Development

2.1. Derivation of New Performance Evaluation Model

For oil/water relative permeability curve, a normalized water saturation can be defined according to the following equation, equivalent to a theoretical recovery ratio.

$$S_{wd} = (S_w - S_{wi}) / (1 - S_{wi}) \quad (2)$$

After analyzing of a large quantity of reservoir relative permeability curves, we found that relative permeability ratio k_{rw}/k_{ro} and normalized water saturation S_{wd} shows a mathematical relation which can be described by equation (3). Figure 2 shows some of the new plots based on examples from real reservoirs.

$$\frac{k_{rw}}{k_{ro}} = \frac{bS_{wd}}{(1 - S_{wd})^n} \quad (3)$$

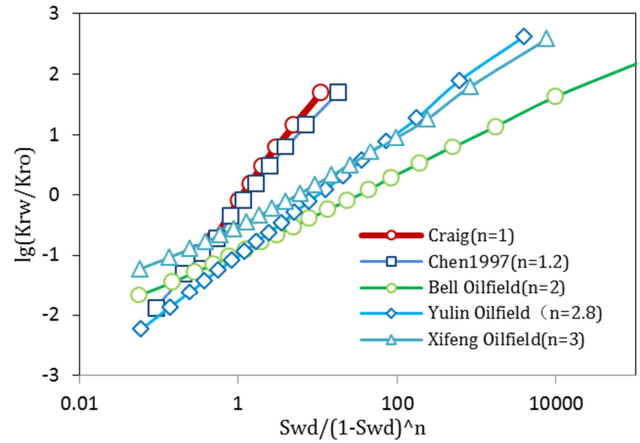


Figure 2. New relative permeability ratio model for different oilfields.

The advantage of this new relative permeability model is that it convert the non-linear characteristic into a new straight line form with two parameters and is capable of depicting the whole life time of the reservoir, no need to distinguish high water-cut period. Based on equation (3) a new water flooding performance model has been developed (as in Appendix 3).

$$\lg(WOR/R) = m - n \lg(E_d - R) \quad (4)$$

In which m and n are constants and n is the same as in the relative permeability ratio, R is recovery ratio, E_d is the waterflood displacing efficiency.

The model in equation (4) can be applied by production history matching based on oil and water production data. A final straight-line can be found by assuming an appropriate displacing efficiency E_d according to representative relative permeability curve or rock core lab test. The ultimate recovery factor E_R can be derived by solving R value in equation (4) when WOR reaches a limit value, such as $WOR=49$. Another application of the new model is to estimate reservoir conformance, or sweep efficiency, according to the definition of recovery factor.

$$E_V = E_R / E_d \quad (5)$$

The steps of using this model are described by following in section 2.2 and Figure 3.

2.2. Steps for Recovery Prediction Based on New Model

(1) Read relative permeability curve data and reservoir production history;

- (2) Normalize k_{rw}/k_{ro} vs. S_{wd} , determine index value of n and displacing efficiency E_d ;
- (3) Do linear regression of WOR/R with (E_d-R) , determine the slope n ;
- (4) Check the two values of n from these two methods, if consistent with each other then go to next step, otherwise adjust or input new relative permeability and assume new E_d value;
- (5) After WOR/R model determined, input the limit value of WOR , solve the R value as ultimate recovery E_R by the WOR/R model, then estimate sweep efficiency by $E_v=E_R/E_d$

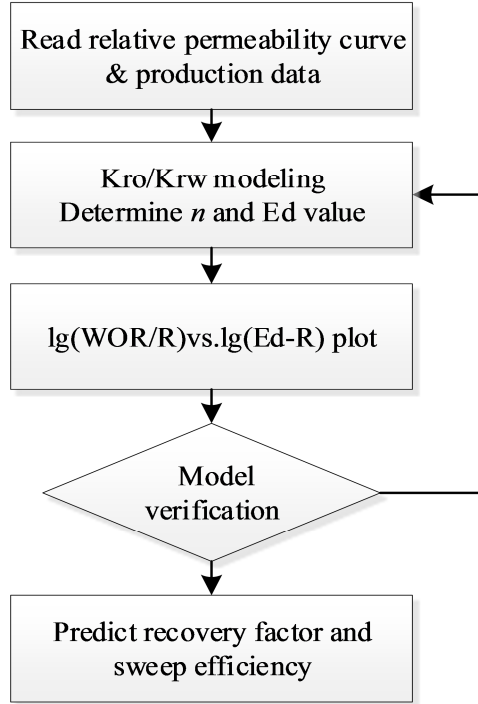


Figure 3. Reservoir performance prediction process with new models.

3. Case Study

3.1. Case Analysis 1: Synthetic Case- Linear Water Drive

A synthetic line-water-drive reservoir is designed with an OOIP of 26.4×10^4 ton. The reservoir permeability is 280 mD and oil viscosity is 20 mPa·s. The reservoir produce under a line water drive with pressure difference of 2MPa and injection-production distance is 500m. The relative permeability and the production performance calculated based on 1D Buckley-Leverett theory are list in Table 2.

Table 2. Relative permeability and production performance in case 1.

S_w/f	k_{ro}/f	k_{rw}/f	f_w/f	$N_p/10^4 t$	R/f
0.5653	0.2399	0.0544	0.6940	13.2231	0.5009
0.5865	0.2016	0.0686	0.7729	13.7512	0.5209
0.6078	0.1666	0.0850	0.8361	14.3533	0.5437
0.6290	0.1349	0.1038	0.8850	14.9807	0.5675
0.6502	0.1066	0.1252	0.9215	15.7830	0.5978
0.6820	0.0704	0.1626	0.9585	16.7038	0.6327
0.7245	0.0337	0.2230	0.9851	17.6594	0.6689
0.7563	0.0150	0.2770	0.9946	18.6697	0.7072

Figure 4 shows the relative permeability curve and k_{ro}/k_{rw} ratio match. It is clear that the mid-term straight-line trend does not exist in the later region of water saturation, indicating two-phase flow nature of high water cut period. The new relative permeability ratio model in this paper provides a good match. Figure 5 shows the match of WOR/R relation and the predicted recovery factor is 70.6% under a limit water-cut value of 99%, which is in high consistency with the theoretical calculation in Table 1.

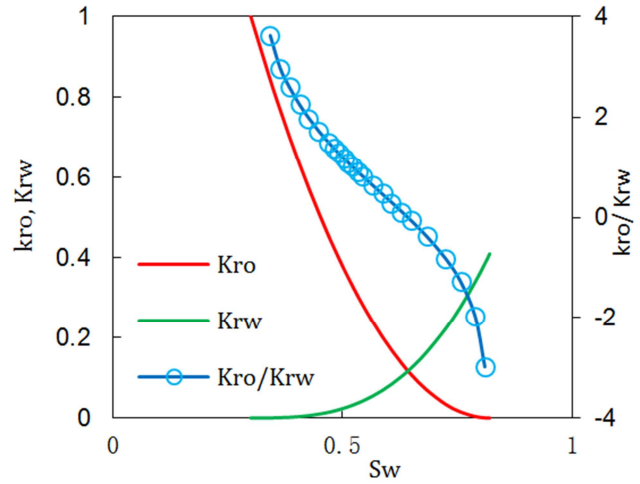


Figure 4. Relative permeability ratio in case 1.

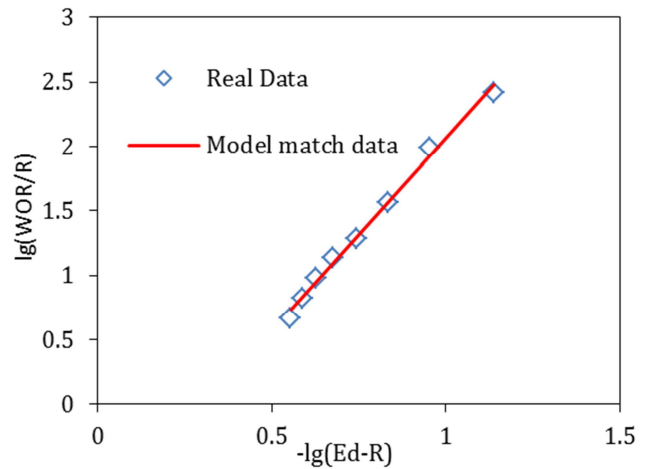


Figure 5. Match of WOR/R model in case 1.

3.2. Case Analysis 2: Gudong Oilfield Performance Analysis

This reservoir is from Gudong Oilfield No7 block which is undergoing a quick water-cut rising after the adjustment in 2003. The water cut is above 95%. By assuming $E_d=0.7$, the WOR/R straight-line relation is derived after history match and the n value is 5.7167, which is consistent with the index value in relative permeability ratio.

$$\lg(WOR/R) = -0.776 - 5.7167 \lg(E_d - R) \quad (6)$$

A recovery factor of 38.6% is obtained by solving R in the

above equation based on a limit value of WOR as 49. This value is close to the recovery factor of 39% derived by Wang [8]. And the sweep efficiency E_v is equal to $0.386/0.7=0.55$, which is very low considering the long water injection history, indicating a high heterogeneity of this reservoir.

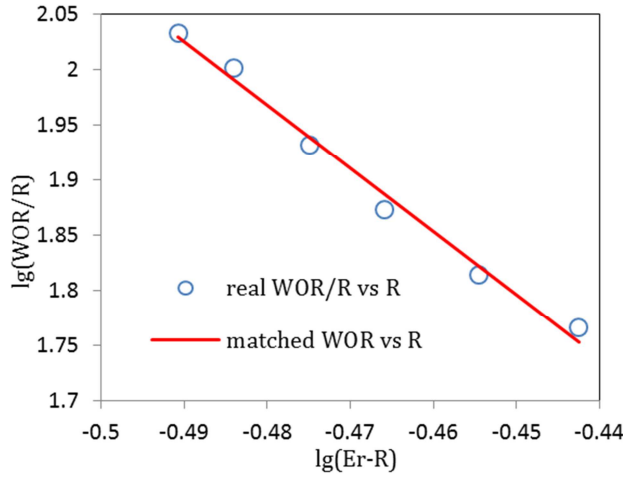


Figure 6. WOR/R relation match of Gudong 7 Block.

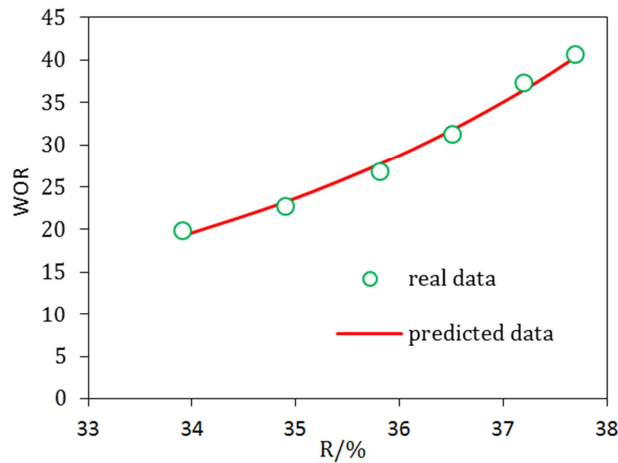


Figure 7. WOR vs R match of Gudong 7 Block.

3.3. Case Analysis 3: Sabei Transition Block

The Sabei transition block is from Daqing oilfield which was analyzed by Chen [9] based on production history. The WOR/R relation is derived according to the new model in this work:

$$\lg(WOR/R) = -0.0149 - 4.4977 \lg(E_d - R) \quad (7)$$

The displacing efficiency E_d is 0.75 from relative permeability curve and the recovery factor from the new model is 40.8%, which is almost close to the result 39.6% given by previous study [9]. The calculated sweep efficiency is 0.544, so effective measures should be considered to improve the water flooding effects in this transition zone. Figure 8 shows the match of WOR/R vs $(E_d - R)$ in equation (7). It is evident that the linear approximation is valid at high water/oil ratio. After convert the WOR to f_w , a good match of

water-cut is shown as in Figure 9.

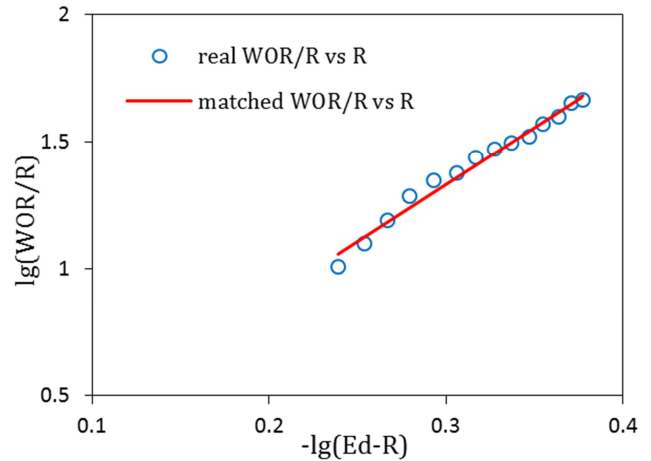


Figure 8. WOR/R relation match of Sabei Block.

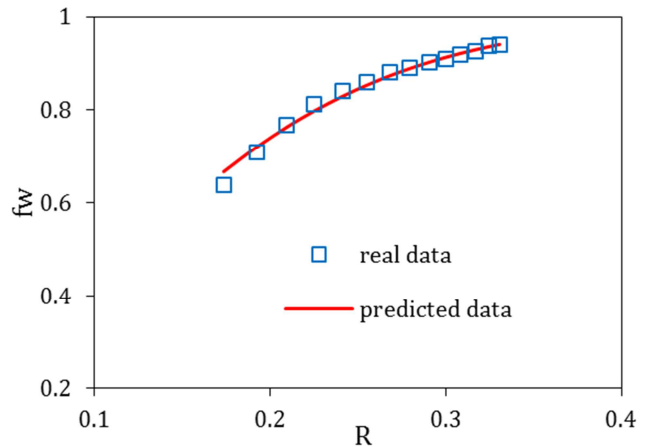


Figure 9. f_w vs R match of Sabei Block.

4. Conclusion

A simple WOR/R water flooding performance analysis technique is developed based on new oil/water relative permeability ratio model which converts the non-linear k_{ro}/k_{rw} relation into a linear expression with limited parameters. The proposed technique in this work provides an effective and useful predictive analysis tool in forecasting ultimate recovery and performance evaluation for mature water flooding reservoirs. The three key indexes for reservoir waterflood performance evaluation, displacing efficiency, recovery factor and sweep efficiency can be estimated simultaneously. Model analysis and field case studies show the benefits of this method in parameter solving and consistency in history matching. The new method has both accuracy and simplicity for performance evaluation of mature oil field in high water-cut period.

Appendix

1. Ershagi and Omeregie “X-plot” model

Ershagi and Omeregie (1978) presented recovery ration and

water cut relation called “X-plot” based on the concepts of fractional flow and the frontal advance theory (Buckley and Leverett).

$$E_r = a_{er} + b_{er}X \quad (8)$$

In which,

$$X = \ln\left(\frac{1}{f_w} - 1\right) - \frac{1}{f_w}, \quad b_{er} = \frac{1}{b(1-S_{wi})}$$

$$a_{er} = -\frac{1}{1-S_{wi}}\left(S_{wi} + \frac{1}{b} \ln C\right), \quad C = a\left(\frac{\mu_w}{\mu_o}\right)$$

The coefficients a and b are obtained from the following empirical relative permeability ratio straight-line relationship.

$$\log(k_{ro}/k_{rw}) = \log(a) + bS_w \quad (9)$$

2. Lo K. WOR vs. N_p relation

Lo (1990) suggested using a logarithm relationship of WOR and N_p

$$\log(WOR) = \frac{b(1-S_{wc})}{OOIP} N_p + \log\left(\frac{a\mu_o}{\mu_w}\right) + bS_{wc} - \frac{1}{\ln 10} \quad (10)$$

In which the constants a and b are determined by the relationship of relative permeability ratio and water saturation, as described by (9).

3. New relative permeability ratio and performance model

Define normalized water saturation S_{wd} ,

$$S_{wd} = \frac{S_w - S_{wi}}{1 - S_{or} - S_{wi}} \quad (11)$$

In which, S_{wi} is the connate water saturation, S_{or} is the residual oil saturation.

A relation of relative permeability ratio and S_{wd} is found by analyzing a large quantity of field examples.

$$\frac{k_{rw}}{k_{ro}} = \frac{bS_{wd}}{(1-S_{wd})^n} \quad (12)$$

In which b and n are two constants which can be determined by data matching.

For water flooding reservoir, the recovery ratio can be defined by:

$$R = \frac{N_p}{N} = \frac{S_w - S_{wi}}{1 - S_{wi}} \quad (13)$$

In which N_p is cumulative oil production, N is the oil in place.

Combining (11) and (13), it gives,

$$R = \frac{1 - S_{or} - S_{wi}}{1 - S_{wi}} S_{wd} \quad (14)$$

In which $(1 - S_{or} - S_{wi})/(1 - S_{wi})$ is the waterflood displacing efficiency which can be expressed as E_d , so we have

$$S_{wd} = \frac{R}{E_d} \quad (15)$$

Under steady state flow, the water-oil ratio is defined as:

$$WOR = \frac{Q_w}{Q_o} = \frac{\mu_o B_o \gamma_w k_{rw}}{\mu_w B_w \gamma_o k_{ro}} \quad (16)$$

Substitute (12) and (15) into (16), it gives:

$$\frac{WOR}{R} = \frac{b\mu_o B_o \gamma_w}{\mu_w B_w \gamma_o} \frac{E_d^{n-1}}{(E_d - R)^n} \quad (17)$$

Take logarithm of (17) on both sides, the final form of the new model is:

$$\lg \frac{WOR}{R} = m - n \lg(E_d - R) \quad (18)$$

$$\text{In which, } m = \lg \frac{b\mu_o B_o \gamma_w E_d^{n-1}}{\mu_w B_w \gamma_o}$$

Where μ_o is oil viscosity, mPa·s, μ_w is water viscosity, mPa·s; B_o is oil formation volume factor, B_w is water formation volume factor; γ_o is surface oil density, g/cm³, γ_w is surface water density, g/cm³; b and n are constants.

Nomenclature

- A, B, C = constants, dimensionless
- E_d = displacing efficiency, fraction
- E_r = oil recovery ratio, fraction
- E_R = ultimate recovery factor, fraction
- E_V = volumetric sweep efficiency, fraction
- f_w = water cut, fraction
- N = Original oil in place (OOIP), m³
- N_p = cumulative oil production, m³
- k_{ro} = oil relative permeability, fraction
- k_{rw} = water relative permeability, fraction
- R = oil recovery ratio, fraction
- S_w = water saturation, fraction
- S_{wd} = normalized water saturation, fraction
- S_{wi} = initial water saturation, fraction
- WOR = water oil ratio, dimensionless
- m, n, b = constants, dimensionless

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